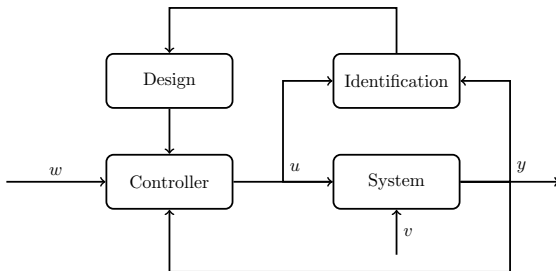




## Lecture Plan

- 1 System theory
- 2 Stochastics
- 3 State estimation 1
- 4 State estimation 2
- 5 Optimal control 1
- 6 System identification 1 + adaptive control 1
- 7 External models + prediction
- 8 Optimal control 2
- 9 Optimal control 3
- 10 System identification 2
- 11 System identification 3 + model validation
- 12 System identification 4 + adaptive control 2
- 13 Adaptive control 3



- Cautious adaptive control
- Dual adaptive control
- Ideas for MSc projects/special courses
- Presentation by Emil Skov Martinsen

## Follow-up from Last Lecture

### CE Self-tuner Adaptive methods

- Explicit adaptive control: Estimate model parameters and then design controller (*explicit design*)
- Implicit adaptive control: Estimate the controller parameters directly (*implicit design*)

### Other terms discussed

- CE: certainty equivalence principle;  $\theta$  replaced by  $\hat{\theta}$
- $J_r = \sum_{i=1}^t (y_i - w_i)^2 \approx \mathbb{E}[(y_i - w_i)^2]t$
- $J_u = \sum_{i=1}^t u_i^2 \approx \mathbb{E}[u_i^2]t$  (requires oscillation around 0)
- $J_e = \sum_{i=1}^t \epsilon_i^2 \approx \sigma^2 t$ , for correct estimation  $\epsilon_i = e_i$
- $J_e \approx J_r$

# Stochastic Adaptive Control - Other Self Tuners

## Follow-up from Last Lecture



Questions?

ARX model with 1-step delay

$$A(q^{-1})y_t = B(q^{-1})u_{t-1} + e_t, \quad e_t \in N_{iid}(0, \sigma^2) \quad (1)$$

Cost function

$$J = \mathbb{E} \left[ \sum_{i=1}^N (y_{t+i} - w_{t+i})^2 \right] \quad (2)$$

Example:  $MV_0$  controller ( $N = 1$ )

$$u_{t-1} = \frac{1}{B}w_t - \frac{S}{B}y_{t-1} = \frac{1}{B}w_t - \frac{q(1-A)}{B}y_{t-1} \quad (3)$$

$$y_t = w_t + e_t \quad (4)$$

Alternative form: System

$$y_t = \phi_t^T \theta + e_t = b_0 u_{t-1} + \varphi_t^T \vartheta + e_t \quad (5)$$

$$\phi_t^T = (-y_{t-1}, -y_{t-2}, \dots, u_{t-1}, u_{t-2}, \dots), \quad \theta^T = (a_1, a_2, \dots, b_0, b_1, \dots) \quad (6)$$

$$\varphi_t^T = (-y_{t-1}, -y_{t-2}, \dots, 0, u_{t-2}, \dots), \quad \vartheta^T = (a_1, a_2, \dots, 0, b_1, \dots) \quad (7)$$

Alternative form: Controller

$$u_{t-1} = \frac{1}{b_0} w_t - \frac{\varphi_t^T \vartheta}{b_0} \quad (8)$$

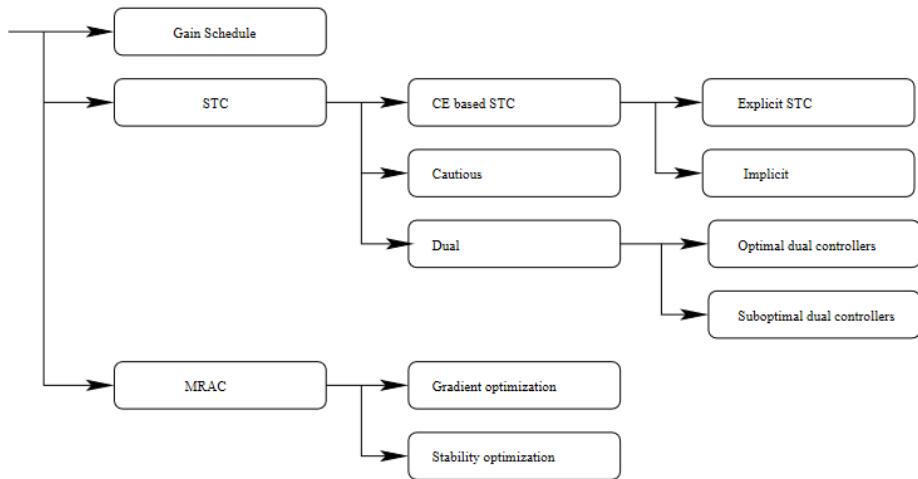
$$y_t = w_t + e_t \quad (9)$$

Relation between  $\phi$  and  $\varphi$

$$\varphi = \phi - \text{diag}(l)\phi, \quad \vartheta = \theta - \text{diag}(l)\theta \quad (10)$$

$$l^T = (0, 0, \dots, 1, 0, \dots) \quad (11)$$

The nonzero entry corresponds to the placement of  $b_0$  and  $u_{t-1}$





Certainty equivalent self-tuner: Use the parameter estimate as the true parameters

$$y_t = \phi_t^T \theta + \epsilon_t, \quad \theta \rightarrow \hat{\theta} \quad (12)$$

Update parameter estimate

$$\epsilon_t = y_t - \phi_t^T \hat{\theta}_{t-1} \quad (13)$$

$$K_t = \frac{P_{t-1} \phi_t}{1 + \phi_t^T P_{t-1} \phi_t} \quad (14)$$

$$\hat{\theta}_t = \hat{\theta}_{t-1} + K_t \epsilon_t \quad (15)$$

$$P_t = P_{t-1} - K_t (1 + \phi_t^T P_{t-1} \phi_t) K_t^T \quad (16)$$

Redesign the control law

$$u_t = \frac{w_{t+1} - S y_t}{R} = \frac{1}{\hat{B}} w_{t+1} - \frac{q(1 - \hat{A})}{\hat{B}} y_t = \frac{1}{\hat{b}_0} w_t - \frac{\varphi_t^T \hat{\vartheta}}{\hat{b}_0} \quad (17)$$

## Cautious adaptive control

**Adaptive Control - Cautious Control**

Cautious adaptive control: Take estimation uncertainty into account

Conditional cost function

$$J = \mathbb{E}[(y_{t+1} - w_{t+1})^2 | Y_t] \quad (18)$$

$$= (\mathbb{E}[y_{t+1} - w_{t+1} | Y_t])^2 + \text{Var}(y_{t+1} - w_{t+1} | Y_t) \quad (19)$$

Uncertainty of parameter estimate

$$\hat{\theta}_t \sim N(\theta, P_t) \quad (20)$$

$$\hat{b}_{0,t} = l^T \hat{\theta}_t \quad (21)$$

$$p_{b,t} = l^T P_t l \quad (22)$$

Control law

$$u_t = \frac{\hat{b}_{0,t}^2}{\hat{b}_{0,t}^2 + p_{b,t}} \left( \frac{w_{t+1} - \varphi_t^T \hat{\theta}}{\hat{b}_{0,t}} - \frac{\varphi_t^T P_t l}{\hat{b}_{0,t}^2} \right) \quad (23)$$

If  $P_t \rightarrow 0$ , cautious control is equivalent to certainty equivalent control

$$u_t = \frac{\hat{b}_{0,t}^2}{\hat{b}_{0,t}^2 + p_{b,t}} \left( \frac{w_{t+1} - \varphi_t^T \hat{\theta}}{\hat{b}_{0,t}} - \frac{\varphi_t^T P_t l}{\hat{b}_{0,t}^2} \right) \rightarrow u_t = \frac{w_{t+1} - \varphi_t^T \hat{\theta}}{\hat{b}_{0,t}} \quad (24)$$

If  $\hat{\theta}_t \rightarrow \theta$ , certainty equivalent control is equivalent to the known control

- 1  $P_t \rightarrow 0$  : Cautious = CE  $\neq$  known
- 2  $\hat{\theta}_t \rightarrow \theta$  : Cautious  $\neq$  CE = known
- 3  $P_t \rightarrow 0, \hat{\theta}_t \rightarrow \theta$  : Cautious = CE = known

### Cautious controller

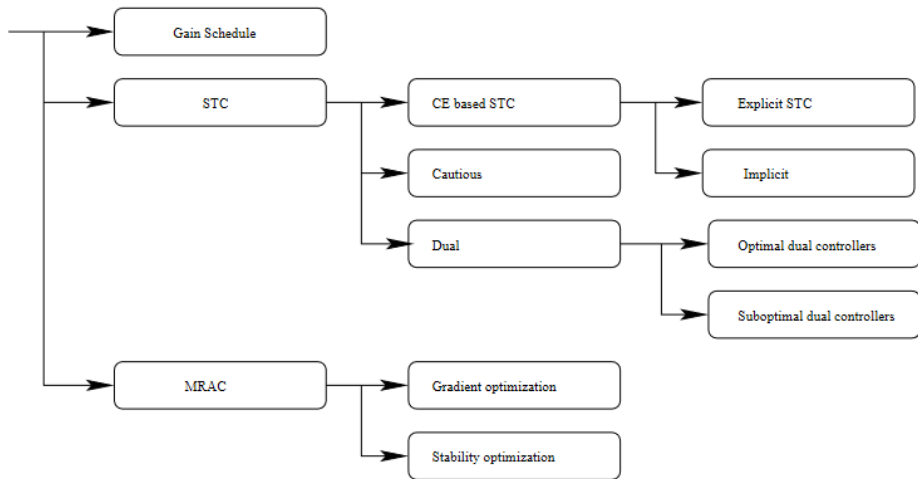
$$u_t = \frac{\hat{b}_{0,t}^2}{\hat{b}_{0,t}^2 + p_{b,t}} \left( \frac{w_{t+1} - \varphi_t^T \hat{\theta}}{\hat{b}_{0,t}} - \frac{\varphi_t^T P_t l}{\hat{b}_{0,t}^2} \right) \quad (25)$$

- *Turn-off phenomenon*: Control is dampened due to high uncertainty of  $b_0$
- Consequence: Less information about  $b_0$  for the next estimate, i.e., the uncertainty increases
- Turn-off usually occurs if  $b_0$  or the control signal is small
- Conclusion: The cautious controller is useful for systems with constant or almost constant parameters, but unsuitable for general time-varying systems

## Examples



Matlab example: Cautious self-tuner



## Dual adaptive control



Dual control: Conditional expectation of the cost

$$J = \min_{U_t} \mathbb{E} \left[ \sum_{i=1}^N (y_{t+i} - w_{t+i})^2 \right] = \mathbb{E}_{Y_t} \left[ \min_{U_t} \mathbb{E} \left[ \sum_{i=1}^N (y_{t+i} - w_{t+i})^2 \middle| Y_t \right] \right] \quad (26)$$

If the parameter uncertainty is Gaussian, the conditional expectation is Gaussian (even if  $y_t$  is not)

$$\xi_t = [\varphi_{t-1}, \hat{\theta}_t, P_t] \quad (27)$$

contains the necessary information

If not Gaussian, it becomes computationally challenging to compute the hyper space and storage requirements increase

Bellman equation

$$V(\xi_t, t) = \min_{u_{t-1}} \mathbb{E}[(y_t - w_t)^2 + V(\xi_{t+1}, t) | Y_{t-1}] \quad (28)$$

The last ( $N$ 'th) step is identical to the cautious controller

$$V(\xi_N, N) = \min_{u_{N-1}} \mathbb{E}[(y_N - w_N)^2 | Y_{N-1}] \quad (29)$$

$$= (\varphi_{N-1}^T \theta_N - w_N)^2 + \sigma^2 + \varphi_{N-1}^T P_N \varphi_{N-1} - \frac{\hat{b}_{0,N} w_N - \varphi_{N-1}^T (\hat{b}_{0,N} \hat{\theta}_N + P_N l)}{\hat{b}_{0,N}^2 - p_{b,N}} \quad (30)$$

substituting into  $V(\xi_{N-1}, N - 1)$ , the second last control can be computed, and so on

This is similar to the LQR – however, it does not have an analytical solution and must be solved numerically

Fundamental paradox of adaptive control

- ① Control objective: Small signals (control action)
- ② Estimation: Large signals (probing action)

For the optimal  $N$ -step dual control problem, the solution is a compromise between these goals

- ① Improved long-term estimation accuracy; sacrificing short-term loss
- ② Probing adds active learning to the method

Cautious control ( $N = 1$ ): The probing effects diminishes and any learning is "accidental"

Issue with dual control: Curse of dimensionality – the computational cost increases drastically with increasing hyperspace dimension and horizon

As optimal dual control is impractical, sub-optimal dual controllers exist. They are based on the cautious controller and fix the issue with turn-off

Various approaches

- ① Constrain the uncertainty
- ② Extend the loss function
- ③ Serial expansion of the loss function
- ④ Add perturbation signals to the control

Constrained one-step controller (minimum distance to zero control)

$$u_t = \begin{cases} u_c & \text{if } |u_c| \geq |u_l| \\ u_l \operatorname{sign}(u_c) & \text{if } |u_c| < |u_l| \end{cases} \quad (31)$$

$u_c$  is the cautious controller input and  $u_l$  is a lower limit determined by us

The constraints do not prevent turn-off, but add extra perturbation when it happens

Alternatively, constrain the uncertainty

$$\text{Tr}(P_{t+1}^{-1}) \geq M \quad (32)$$

or constrain only  $p_b$

$$p_{b,t+1} \leq \begin{cases} \gamma \hat{b}_{0,t+1}^2 & \text{if } p_{b,t} \leq \hat{b}_{0,t}^2 \\ \alpha p_{b,t} & \text{otherwise} \end{cases} \quad (33)$$

Add uncertainty to the cost function

$$J = \mathbb{E}[(y_{t+1} - w_{t+1})^2 + \rho f(P_{t+1})] \quad (34)$$

$f$  can be formulated in many ways

- 1  $f(P_{t+1}) = p_{b,t+1}$
- 2  $f(P_{t+1}) = R_2 \frac{p_{b,t+1}}{p_{b,t}}$
- 3  $f(P_{t+1}) = -\frac{\det(P_t)}{\det(P_{t+1})}$
- 4  $f(P_{t+1}) = -\epsilon_{t+1}^2$

This might lead to multiple local minima, and numerical optimization is required. Alternatively, use a second order serial expansion (e.g., a Taylor expansion)

**Sub-Optimal Dual control - Extended Loss Function - Example**

Third version of  $f$

$$J = \mathbb{E} \left[ (y_{t+1} - w_{t+1})^2 - \rho \frac{\det(P_t)}{\det(P_{t+1})} \middle| Y_t \right] \quad (35)$$

Ratio between determinants

$$\frac{\det(P_t)}{\det(P_{t+1})} = 1 + \phi_{t+1}^T P_t \phi_{t+1} \quad (36)$$

Analytical control law

$$u_t = \frac{\hat{b}_0(w_{t+1} - \varphi_{t+1}^T \hat{v}_t) + \rho(P_t l)^T \varphi_{t+1}}{\hat{b}_0^2 - \rho p_{b,t}} \quad (37)$$

Depending on  $\rho$ , we get specific controllers

- 1  $\rho = 0$ : the CE controller
- 2  $\rho = -1$ : the cautious controller
- 3  $\rho > 0$ : an active learning controller



Add probing/perturbation signal

$$u_t = u_t^c + u_t^x \quad (38)$$

Possible probing/perturbation signals include

- 1 PRBS
- 2 DOX: Design of excitation signal

They can be applied both at certain points in time (low uncertainty) or constantly

Questions?

- 34746 – Robust & fault-tolerant control
- 34791 – Topics in advanced control (PhD)
- 02619 – Model predictive control
- 02417 – Time series analysis
- 02427 – Advanced time series analysis

## Subjects for special courses and MSc projects

Bilinear systems (e.g., in heat exchangers)

$$x_{k+1} = Ax_k + Bu_k + G(x_k \otimes u_k) \quad (39)$$

Separable bilinear systems (e.g., in district heating)

$$x_{k+1} = Ax_k + Bu_k + G(x_k \otimes v_k) \quad (40)$$

Quadratic-bilinear systems (e.g., in nuclear fission)

$$x_{k+1} = Ax_k + bu_k + H(x_k \otimes x_k) + G(x_k \otimes u_k) \quad (41)$$

- TCLab device
- Electrolysis
- Tank systems
- ... or others

## Control of systems with time delays

Can both be discrete- and continuous-time

- Ordinary differential equations (ODEs)

$$\dot{x}(t) = f(x(t), u(t), d(t), \theta)$$

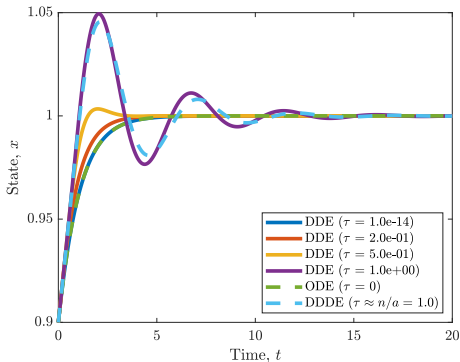
- Delay differential equations (DDEs)  
with absolute delays

$$\dot{x}(t) = f(x(t), x(t - \tau), u(t), d(t), \theta)$$

- Distributed delay differential equations (DDDEs)

$$\dot{x}(t) = f(x(t), z(t), u(t), d(t), \theta),$$

$$z(t) = \int_{-\infty}^t \alpha(t - s)x(s) ds$$



Potential collaboration with Prof. John Wyller from NMBU, Norway.

DAEs

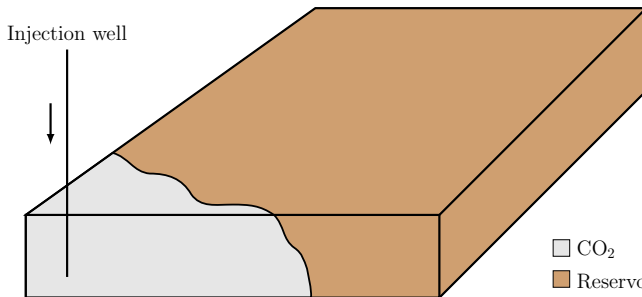
$$\begin{aligned}\dot{x}(t) &= F(y(t), u(t), d(t), \theta), \\ 0 &= G(x(t), y(t), z(t), \theta)\end{aligned}$$

Equilibrium 1/2

$$\begin{aligned}\min_{y(t)} \quad & f(y(t)), \\ \text{s.t.} \quad & g(y(t)) = x(t), \\ & h(y(t)) = 0\end{aligned}$$

Equilibrium 2/2

$$\begin{aligned}\min_{y(t)} \quad & f(y(t)), \\ \text{s.t.} \quad & g(y(t)) = x(t), \\ & h(y(t)) = 0, \\ & y(t) \geq 0\end{aligned}$$



- CO<sub>2</sub> storage
- Geothermal energy
- Power-to-X

*Potential collaborations with*

*SemperCycle ApS, Nordic Hydrogen*

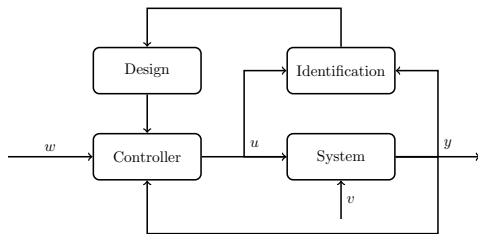
*ApS, and MPI Magdeburg, Germany.*

□ CO<sub>2</sub>

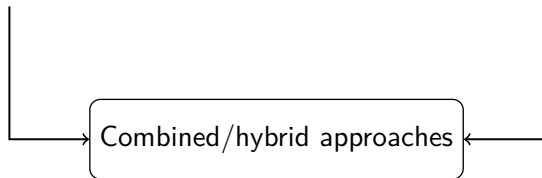
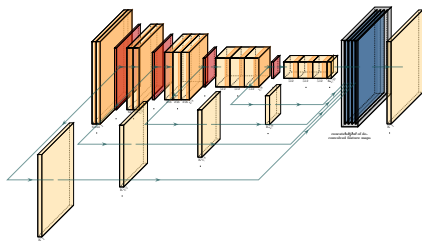
■ Reservoir fluid



### Stochastic adaptive control



### Reinforcement learning



# Model reduction and numerical methods for optimal control

The linear continuous-time system

$$\dot{x}(t) = Ax(t) + Bu(t),$$

$$y(t) = Cx(t) + Du(t),$$

reduces to

$$\dot{\hat{x}}(t) = A_r \hat{x}(t) + B_r u(t),$$

$$\hat{y}(t) = C_r \hat{x}(t) + D_r u(t).$$

What about

$$\dot{x}(t) = f(x(t), u(t))$$

and optimal control/dynamic optimization problems?

Original system

$$\dot{x} = A x + B u$$

$$y = C x + D u$$

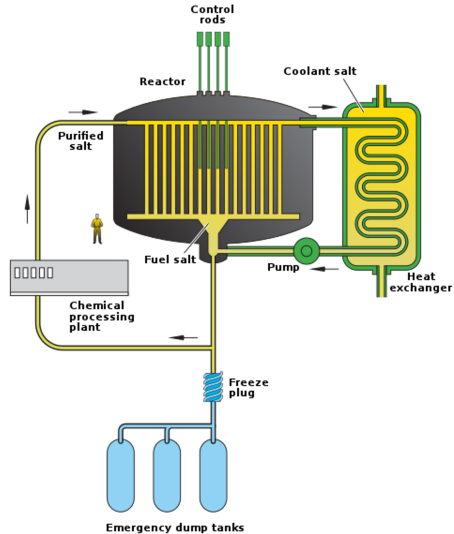
Reduced system

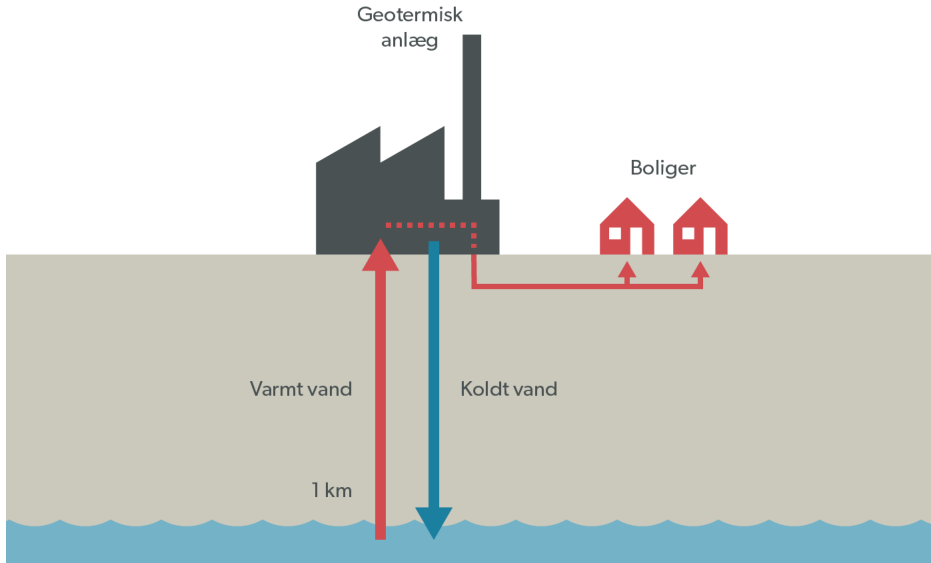
$$\dot{\hat{x}} = A_r \hat{x} + B_r u$$

$$\hat{y} = C_r \hat{x} + D_r u$$

# Stochastic Adaptive Control - Other Self Tuners

## Nuclear fission





# Stochastic Adaptive Control - Other Self Tuners

## Power grids

